

Robust Constrained Control for Driver-Automation Shared Driving of Intelligent Vehicles

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Outline

- ① **Context and challenges**
- ② **Human-in-the-loop control design**
 - **System modeling**
 - **Description of the proposed method**
 - **Control design**
- ③ **Illustrative experimental results**
- ④ **Concluding Remarks**

Context



- ◎ Human drivers are responsible 90% road accidents^[1]
- ◎ Automation can help to reduce the workload and the human errors
- ◎ Full automation of vehicle could be possible!

Google Driverless Car



Context

◎ Why not full automation of the driving task?

- Unpredictable environments (outside the operating range of the automation)



Loss of GPS signal



Presence of undetected obstacle

Absence of markings on the ground

Human capacities (creativity and insight) are still needed!

Challenging Issue

◎ Human-machine system



Question: “How could we combine the best of the human and machine?”

Principle of cooperative control^[1]

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Vehicle Modeling for Control Design

Three types of system dynamics^[1]

- Vehicle dynamics (or linear bicycle model)

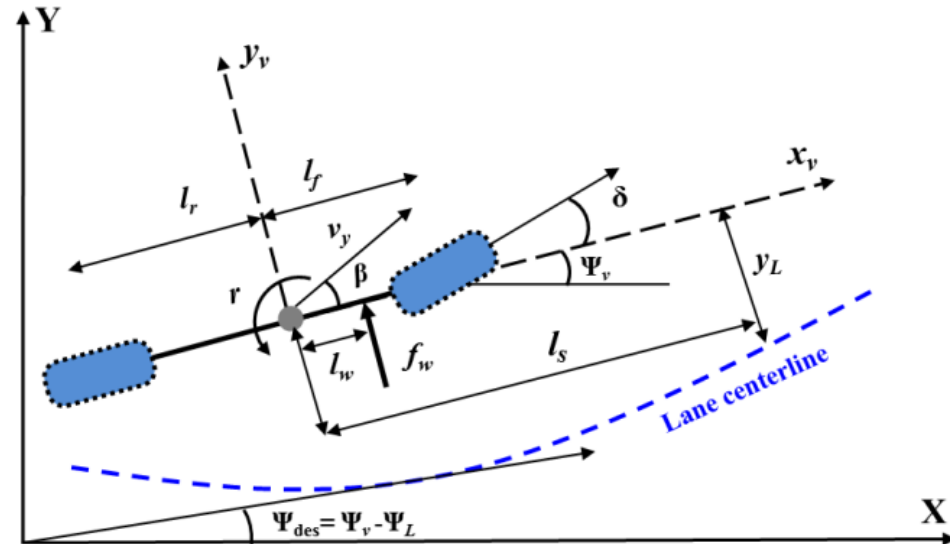
$$\begin{bmatrix} \dot{\beta} \\ \dot{r} \end{bmatrix} = \begin{bmatrix} a_{11} & a_{12} \\ a_{21} & a_{22} \end{bmatrix} \begin{bmatrix} \beta \\ r \end{bmatrix} + \begin{bmatrix} b_1 \\ b_2 \end{bmatrix} \delta + \begin{bmatrix} e_1 \\ e_2 \end{bmatrix} f_w$$

- Road-vehicle positioning

$$\begin{cases} \dot{y}_L = v_x \beta + l_s r + v_x \psi_L \\ \dot{\psi}_L = r - v_x \rho_r \end{cases}$$

- Steering system

$$\ddot{\delta}_d = \frac{T_{s\beta}}{I_s} \beta + \frac{T_{sr}}{I_s} r - \frac{T_{s\beta}}{R_s I_s} \delta_d - \frac{B_s}{I_s} \dot{\delta}_d + \frac{1}{I_s} (T_c + T_d)$$



Vehicle Modeling for Control Design

Road-vehicle control-based model

① Lateral vehicle dynamics

② Lane keeping dynamics

③ Steering system model

$$\dot{x} = A \downarrow v (v \downarrow x) x + B \downarrow u (T \downarrow c + T \downarrow d) + B \downarrow w (v \downarrow x) w$$

- System state

$$x = [v \downarrow y \quad r \quad \psi \downarrow L \quad y \downarrow L \quad \delta \quad \delta]^\top$$

- Control input

$$v = T \downarrow c + T \downarrow d$$

- System disturbance

$$w = [f \downarrow w \quad \rho \downarrow r]$$

$v \downarrow y$ lateral speed

r yaw rate

$y \downarrow L$ lateral offset

$\psi \downarrow L$ heading error

δ steering angle

δ steering speed

Vehicle Modeling for Control Design

◎ Road-vehicle model

$$\dot{x} = A_v (v \downarrow x) x + B_u (T \downarrow c + T \downarrow d) + B_w (v \downarrow x) w$$

⇒ Conflict issue

◎ Simplified driver model^[1]

$$T \downarrow d = K \downarrow d1 \theta \downarrow near + K \downarrow d2 \theta \downarrow far$$

- Driver tracking performance

$$\theta \downarrow near = y \downarrow L / v \downarrow x T \downarrow p + \psi \downarrow L$$

- Driver anticipatory behaviors

$$\theta \downarrow far = \theta \downarrow 1 v \downarrow y + \theta \downarrow 2 r + \theta \downarrow 3 \delta$$

⇒ Driver torque = linear combination of system states

◎ Driver-in-the-loop-vehicle model

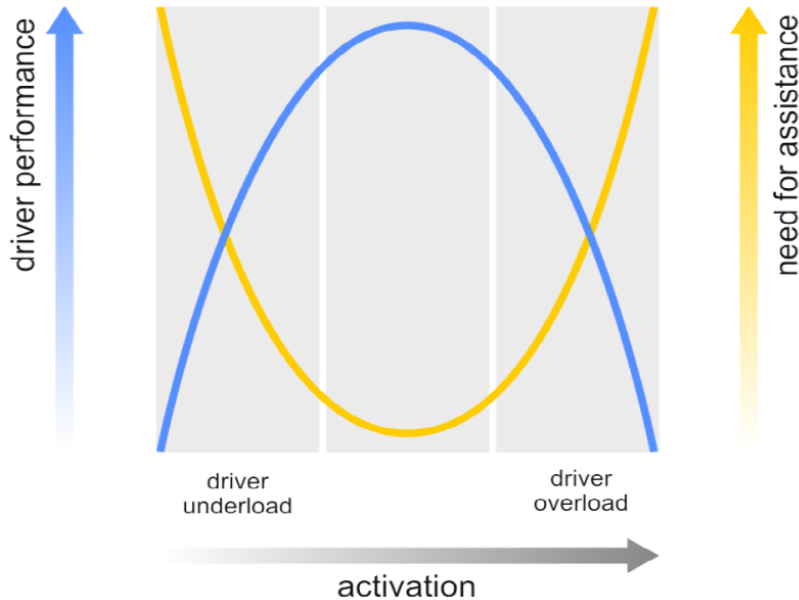
$$\dot{x} = A_v \dot{x} + B_u (T \downarrow c + T \downarrow d) + B_w w$$

—————→
Driver model

$$\dot{x} = Ax + Bu T \downarrow c + Bw w$$

Shared Driving Control Strategy

Need for assistance w.r.t. driver load and performance



U-shape function^[2]

Principle of cooperative control^[1]

- ⇒ The assistance should relieve the driver in underload and overload conditions.
- ⇒ The driver is always in the control loop.
- ⇒ There should have a continuous feedback between the automation system and the driver

Proposed solution

$$T_{\downarrow c} = \mu(\theta_{\downarrow d})u$$

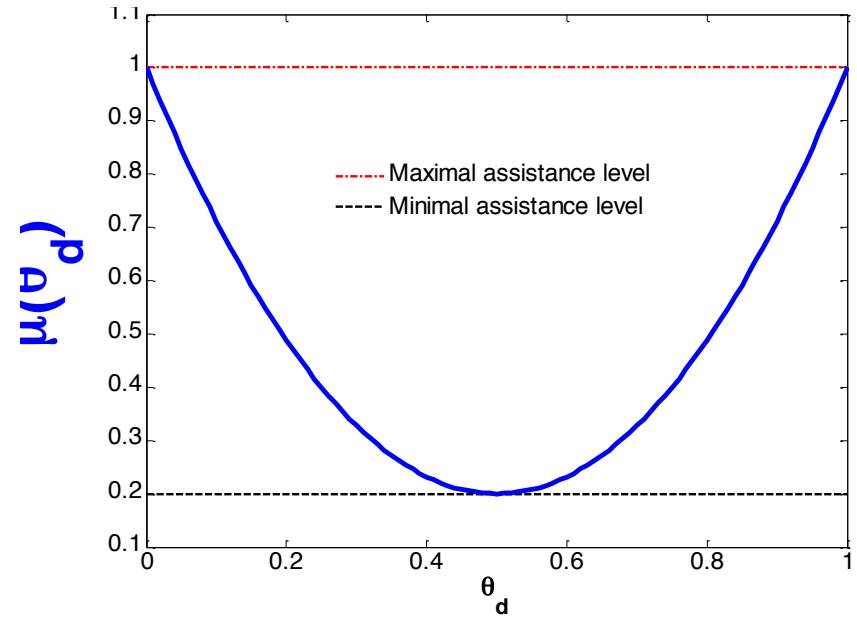
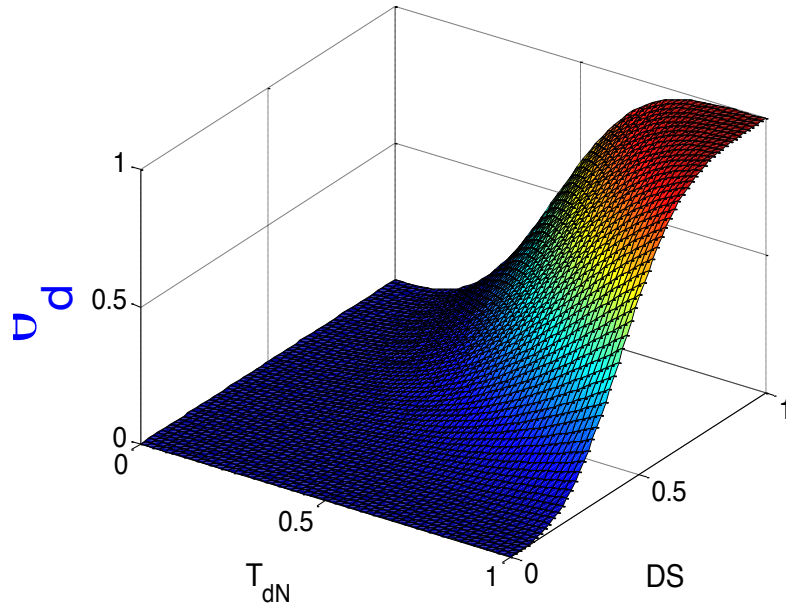
$\theta_{\downarrow d}$: driver activity variable

u : fictive torque to be designed



Shared Driving Control Strategy

Need for assistance w.r.t. driver load and performance



Control-based model

$$\dot{x} = Ax + B \downarrow u \quad T \downarrow c + B \downarrow w \quad w$$

$$\downarrow T \downarrow c = \mu(\theta \downarrow d) u$$

$$\dot{x} = A(\mu(\theta \downarrow d), v \downarrow x) x + B \downarrow u (\mu(\theta \downarrow d)) u + B \downarrow w (v \downarrow x) w$$

Takagi-Sugeno model-based control technique

Takagi-Sugeno Model-Based Control Design

◎ Takagi-Sugeno modeling^[1] for quasi-LPV systems

$$\dot{x} = A(\theta)x + B_1 u(\theta) \text{sat}(u) + B_2 w(\theta)w \quad \rightarrow \quad \dot{x} = \sum_{i=1}^r \eta_i(\theta) (A_i x + B_i u(\theta) \text{sat}(u) + B_i w)$$

- r : number of linear models
- Membership functions $\eta_i(\theta) \geq 0$, $\sum_{i=1}^r \eta_i(\theta) = 1$
- Takagi-Sugeno fuzzy system = **convex combination** of linear subsystems

Constrained Takagi-Sugeno Control Design

◎ PDC (Parallel Distributed Compensation) control law^[1]

$u = \sum_{i=1}^r \eta_i(\theta) K_i x$ ⇒ Same membership functions as T-S model

◎ System constraints $u_{\min} \leq u \leq u_{\max}, Cx \leq d$

- Unavoidable in almost real-world applications

☹ **Degrade the system performance**

☹ **May make the system unstable**

- How to deal with it? ⇒ **Concept of robust invariant sets^[2]**

Constrained Takagi-Sugeno Control Design

Control task: Design an input-unsaturated PDC controller

- Property 1: State constraints

Closed-loop system states remains in the polyhedral region

$$x \in \mathcal{D} \downarrow x = \{x \in \mathbb{R}^n \uparrow n \downarrow x : M \downarrow(k) x \leq 1, k \in \{1, \dots, q\}\}$$

- Property 2: Regional quadratic α -stability

When $w=0$, exponential convergence to the origin with a decay rate α

$$\mathbb{V}(x) < -2\alpha \mathbb{V}(x), \mathbb{V}(x) = x \uparrow \uparrow P x, P > 0$$

- Property 3: $\mathcal{L} \downarrow \infty$ performance

When $w \neq 0$, the trajectories remain in the estimate domain of attraction and

$$z(t) \uparrow \uparrow z(t) \leq \gamma, \forall w \in \mathcal{W} \downarrow \rho$$

Constrained Takagi-Sugeno Control Design

◎ Sector condition for control input saturation^[1]

Consider $K_{li} \in \mathbb{R}^{n_u \times n_x}$ and $G_{li} \in \mathbb{R}^{n_u \times n_x}$, $i \in \Omega_r$. Define $\psi(u) = u - \text{sat}(u)$

and

$$\mathcal{D}_u = \{x \in \mathbb{R}^{n_x} : |\sum_{i=1}^r \eta_{li}(\theta) (K_{li}(l) - G_{li}(l))x| \leq u_{\max}(l), l \in \Omega_{n_u}\}$$

If $x \in \mathcal{D}_u$, then

$$\psi(u)^T (\sum_{i=1}^r \eta_{li}(\theta) S_{li})^{-1} [\psi(u) - \sum_{i=1}^r \eta_{li}(\theta) G_{li} x] \leq 0$$



Incorporated into Lyapunov stability condition

◎ And some other results on inclusion conditions $x \in \mathcal{D}_x$, $x \in \mathcal{D}_u$

Constrained Takagi-Sugeno Control Design

How to design such a controller?

Theorem: If there exist $X, S_i, V_i, X_{21}^j, \dots$, and positive scalars τ_1, τ_2, ρ such that

1. $[X^* @ V_i(l) - W_i(l) \otimes \max(l) \tau_2] \geq 0$
2. $[X^* @ M(k) \otimes X \otimes \max(l) \tau_2] \geq 0$
3. $[X^* @ C_i X + \gamma I] \geq 0$
4. $\{\Psi_{ii} < 0, \quad i \in \{1, \dots, r\}\}$
5. $\tau_1 - \tau_2 \rho > 0$

$$\Psi_{ij} = \text{He} \begin{bmatrix} \Psi_{ij(1,1)} & B_i^u X_{32}^j & B_i^u X_{33}^j & -B_i^u S_j & B_i^w \\ \Psi_{ij(2,1)} & -X_{22}^j & -X_{23}^j & 0 & 0 \\ \Psi_{ij(3,1)} & -X_{32}^j & -X_{33}^j & 0 & 0 \\ W_i & 0 & 0 & -S_j & -S_j \\ 0 & 0 & 0 & 0 & -\tau_2 I/2 \end{bmatrix}$$

$$\Psi_{ij(1,1)} = A_i X + B_i^u X_{31}^j + \tau_1 X/2$$

$$\Psi_{ij(2,1)} = C_i X - X_{21}^j$$

$$\Psi_{ij(3,1)} = V_i - X_{31}^j$$

Feedback control gains

$$K_i = V_i X^{-1}, \quad i \in \{1, \dots, r\}$$

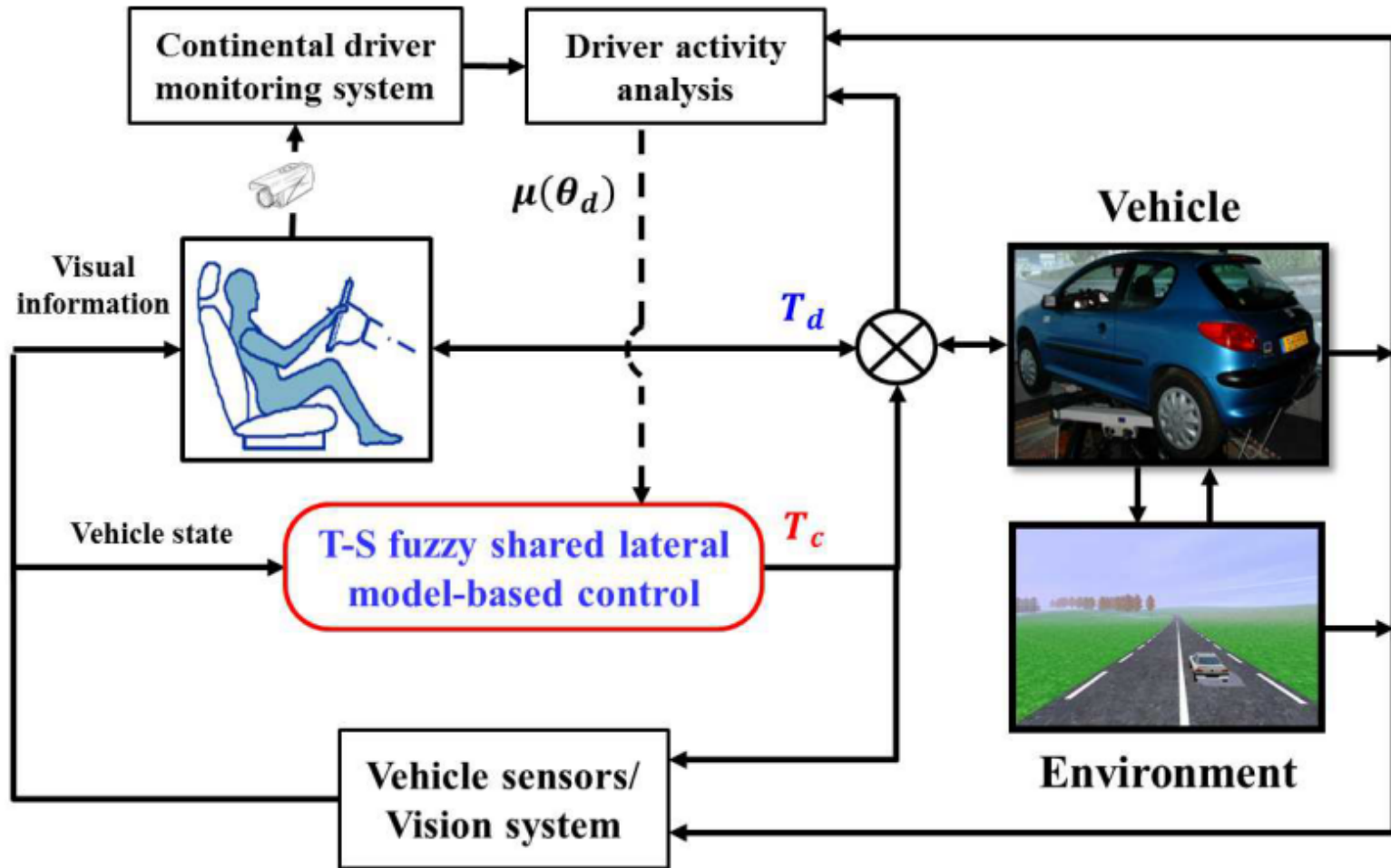


LMI formulation

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Hardware Experiments

Experimental setup: LAMIH-SHERPA interactive driving simulator

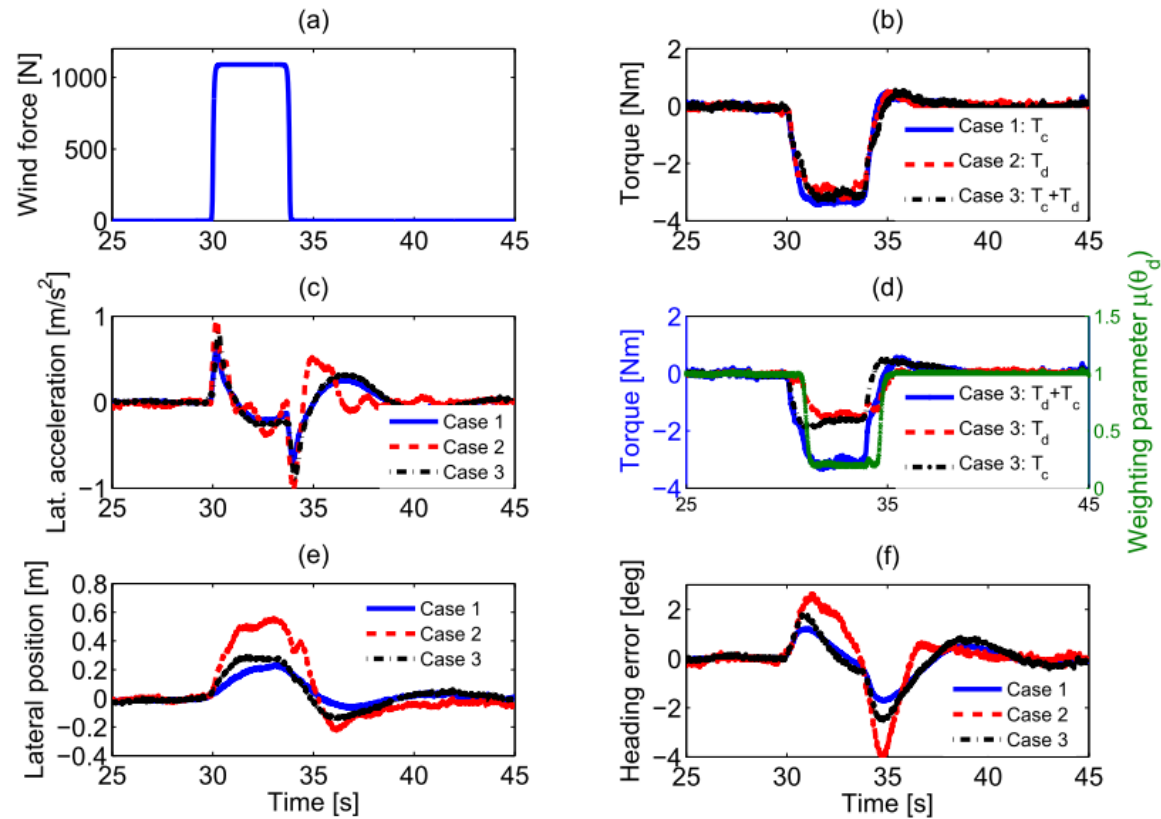


Hardware Experiments

Test 1: Disturbance rejection (straight road, $v \downarrow x = 15 \text{ m/s}$, $f \downarrow w = 1100 \text{ N}$)

Case 1: Automatic ($T \downarrow d = 0$), Case 2: Manual ($T \downarrow c = 0$), Case 3: Shared control

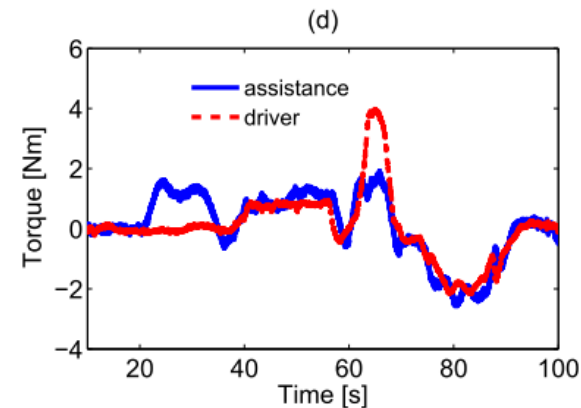
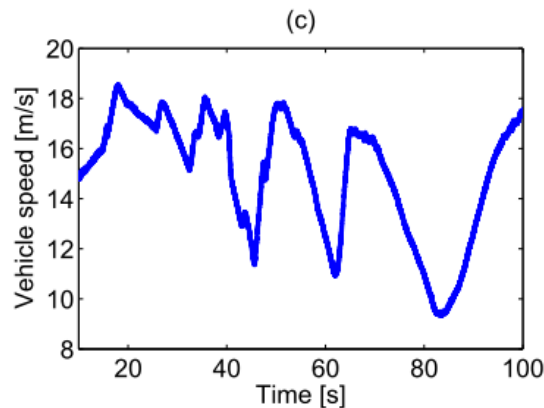
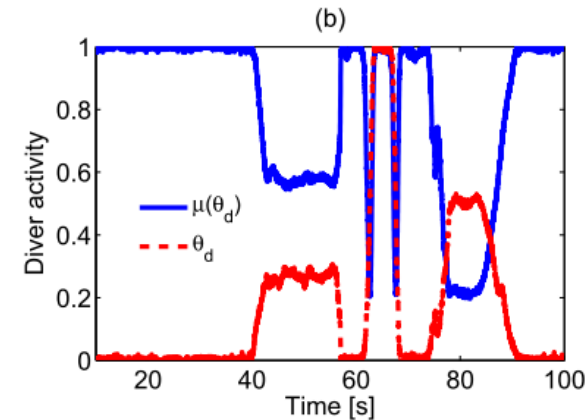
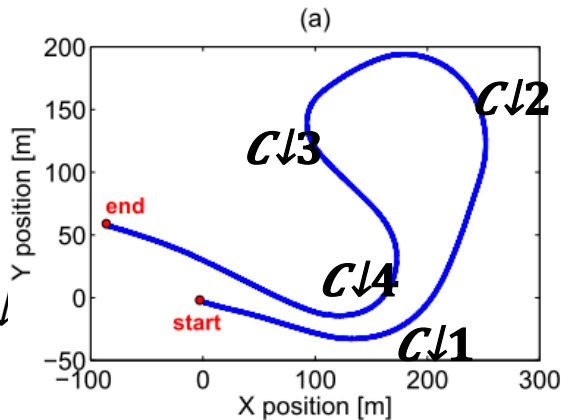
- Similar steering torques
- Small tracking errors
- Only 50% driver's effort for Case 3
- Shared control without conflict



Hardware Experiments

Test 2: Driving task with an adaptive level of assistance

- Phase 1 (10s to 40s): automatic $C\downarrow$
- Phase 2 (40s to 60s): shared $C\downarrow 2$
- Phase 3 (60s to 70s): shared $C\downarrow 3$
- Phase 4 (70s to 100s): shared $C\downarrow 4$



Lane-keeping without driver-automation conflict

Many other tests and performance evaluation can be found here:

Anh-Tu Nguyen, Chouki Sentouh, Jean-Christophe Popieul, "Driver-Automation Cooperative Approach for Shared Steering Control under Multiple System Constraints: Design and Experiments", *IEEE Transactions on Industrial Electronics*, vol. 64, issue 5, pp. 3819-3830, 2017 [IF=7.168].

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Concluding Remarks



◎ **Conclusion:** Novel approach for vehicle shared driving control

- Online adaptation of the control authority according to driver's activity
- Takagi-Sugeno approach \Rightarrow driver's activity variable and vehicle speed variation
- Consideration of system constraints to improve the control performance
- Experimental validation with the SHERPA driving simulator and a human driver

◎ **Current investigations**

- Sensor reduction for shared control under system constraints
- Combined longitudinal-lateral shared control

THANK YOU FOR YOUR ATTENTION !

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Hardware Experiments

Test 3: Emergency double lane change maneuver

- Case 1: *adaptive* authority allocation
- Case 2: *constant* authority allocation
- Small driver's effort with Case 1
- Control input saturation in Case 2

